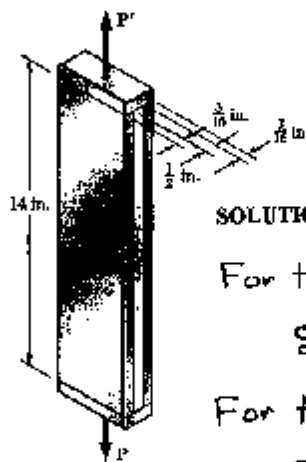


PROBLEM 2.116



2.111 Two tempered-steel bars, each  $\frac{1}{16}$ -in. thick, are bonded to a  $\frac{1}{2}$ -in. mild-steel bar. This composite bar is subjected as shown to a centric axial load of magnitude  $P$ . Both steels are elastoplastic with  $E = 29 \times 10^6$  psi and with yield strengths equal to 100 ksi and 50 ksi, respectively, for the tempered and mild steel.

\*2.116 For the composite bar in Prob. 2.111, determine the residual stresses in the tempered-steel bars if  $P$  is gradually increased from zero until the deformation of the bar reaches a maximum value  $\delta_m = 0.04$  in. and is then decreased back to zero.

SOLUTION

For the mild steel  $A_1 = (\frac{1}{2})(2) = 1.00 \text{ in}^2$

$$S_{Y1} = \frac{L \sigma_{Y1}}{E} = \frac{(14)(50 \times 10^3)}{29 \times 10^6} = 0.024138 \text{ in}$$

For the tempered steel  $A_2 = 2(\frac{3}{16})(2) = 0.75 \text{ in}^2$

$$S_{Y2} = \frac{L \sigma_{Y2}}{E} = \frac{(14)(100 \times 10^3)}{29 \times 10^6} = 0.048276 \text{ in}$$

Total area:  $A = A_1 + A_2 = 1.75 \text{ in}^2$

$S_{Y1} < S_m < S_{Y2}$  The mild steel yields. Tempered steel is elastic.

Forces  $P_1 = A_1 \sigma_{Y1} = (1.00)(50 \times 10^3) = 50 \times 10^3 \text{ lb}$

$$P_2 = \frac{E A_2 S_m}{L} = \frac{(29 \times 10^6)(0.75)(0.04)}{14} = 62.14 \times 10^3 \text{ lb}$$

Stresses  $\sigma_1 = \frac{P_1}{A_1} = \sigma_{Y1} = 50 \times 10^3 \text{ psi}$

$$\sigma_2 = \frac{P_2}{A_2} = \frac{62.14 \times 10^3}{0.75} = 82.86 \times 10^3 \text{ psi}$$

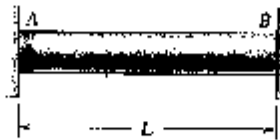
Unloading  $\sigma' = \frac{P}{A} = \frac{112.14}{1.75} = 64.08 \times 10^3 \text{ psi}$

Residual stresses

$$\begin{aligned} \sigma_{1, \text{res}} &= \sigma_1 - \sigma' = 50 \times 10^3 - 64.08 \times 10^3 = -14.08 \times 10^3 \text{ psi} \\ &= -14.08 \text{ ksi} \end{aligned}$$

$$\begin{aligned} \sigma_{2, \text{res}} &= \sigma_2 - \sigma' = 82.86 \times 10^3 - 64.08 \times 10^3 = 18.78 \times 10^3 \text{ psi} \\ &= 18.78 \text{ ksi} \end{aligned}$$

PROBLEM 2.117



2.117 A uniform steel rod of cross-sectional area \$A\$ is attached to rigid supports and is unstressed at a temperature of \$8^\circ\text{C}\$. The steel is assumed to be elastoplastic with \$\sigma\_y = 250\text{ MPa}\$ and \$G = 200\text{ GPa}\$. Knowing that \$\alpha = 11.7 \times 10^{-6}/^\circ\text{C}\$, determine the stress in the bar (a) when the temperature is raised to \$165^\circ\text{C}\$; (b) after the temperature has returned to \$8^\circ\text{C}\$.

SOLUTION

Determine temperature change to cause yielding

$$S = -\frac{PL}{AE} + L\alpha(\Delta T) = -\frac{\sigma_y L}{E} + L\alpha(\Delta T)_y = 0$$

$$(\Delta T)_y = \frac{\sigma_y}{E\alpha} = \frac{250 \times 10^6}{(200 \times 10^9)(11.7 \times 10^{-6})} = 106.838^\circ\text{C}$$

But  $\Delta T = 165 - 8 = 157^\circ\text{C}$

(a) Yielding occurs =  $\sigma = -\sigma_y = -250\text{ MPa}$  ←

Cooling  $(\Delta T)' = 157^\circ\text{C}$

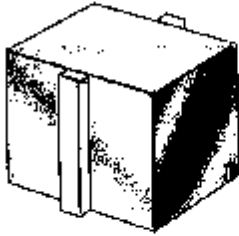
$$S' = S'_p + S'_t = -\frac{P'L}{AE} + L\alpha(\Delta T)' = 0$$

$$\sigma' = \frac{P'}{A} = -E\alpha(\Delta T)'$$

$$= -(200 \times 10^9)(11.7 \times 10^{-6})(157) = -367.38 \times 10^6\text{ Pa}$$

(b)  $\sigma_{res} = -\sigma_y + \sigma' = -250 \times 10^6 + 367.38 \times 10^6 = 117.38 \times 10^6\text{ Pa}$   
 $= 117.4\text{ MPa}$  ←

PROBLEM 2.118



2.118 A narrow bar of aluminum is bonded to the side of a thick steel plate as shown. Initially, at  $T_1 = 20^\circ\text{C}$ , all stresses are zero. Knowing that the temperature will be slowly raised to  $T_2$  and then reduced to  $T_1$ , determine (a) the highest temperature  $T_2$  that does not result in residual stresses, (b) the temperature  $T_2$  that will result in a residual stress in the aluminum equal to  $100\text{ MPa}$ . Assume  $\alpha_s = 23.6 \times 10^{-6}/^\circ\text{C}$  for the aluminum and  $\alpha_a = 11.7 \times 10^{-6}/^\circ\text{C}$  for the steel. Further assume that the aluminum is elastoplastic, with  $E = 70\text{ GPa}$  and  $\sigma_y = 100\text{ MPa}$ . (Hint: Neglect the small stresses in the plate.)

SOLUTION

Determine temperature change to cause yielding

$$s = \frac{PL}{EA} + L\alpha_a(\Delta T)_y = L\alpha_s(\Delta T)_y$$

$$\frac{P}{A} = \sigma = -E(\alpha_a - \alpha_s)(\Delta T)_y = -\sigma_y$$

$$(\Delta T)_y = \frac{\sigma_y}{E(\alpha_a - \alpha_s)} = \frac{100 \times 10^6}{(70 \times 10^9)(23.6 - 11.7)(10^{-6})} = 120.04^\circ\text{C}$$

$$(a) \quad T_{2y} = T_1 + (\Delta T)_y = 20 + 120.04 = 140.04^\circ\text{C}$$

After yielding

$$s = \frac{\sigma_y L}{E} + L\alpha_a(\Delta T) = L\alpha_s(\Delta T)$$

Cooling

$$s' = \frac{P'L}{AE} + L\alpha_a(\Delta T) = L\alpha_s(\Delta T)'$$

The residual stress is

$$\sigma_{res} = \sigma_y - \frac{P'}{A} = \sigma_y - E(\alpha_a - \alpha_s)(\Delta T)'$$

$$\text{Set } \sigma_{res} = -\sigma_y$$

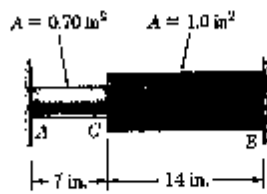
$$-\sigma_y = \sigma_y - E(\alpha_a - \alpha_s)(\Delta T)'$$

$$\Delta T' = \frac{2\sigma_y}{E(\alpha_a - \alpha_s)} = \frac{(2)(100 \times 10^6)}{(70 \times 10^9)(23.6 - 11.7)(10^{-6})} = 240.1^\circ\text{C}$$

$$(b) \quad T_2 = T_1 + \Delta T' = 20 + 240.1 = 260.1^\circ\text{C}$$

If  $T_2 > 260.1^\circ\text{C}$ , the aluminum bar will most likely yield in compression.

**PROBLEM 2.119**



2.119 The steel rod  $ABC$  is attached to rigid supports and is unstressed at a temperature of  $38^\circ\text{F}$ . The steel is assumed elastoplastic, with  $\sigma_y = 36 \text{ ksi}$  and  $E = 29 \times 10^4 \text{ psi}$ . The temperature of both portions of the rod is then raised to  $250^\circ\text{F}$ . Knowing that  $\alpha = 6.5 \times 10^{-6}/^\circ\text{F}$ , determine (a) the stress in portion  $AC$ , (b) the deflection of point  $C$ .

**SOLUTION**

$$\delta_{B/A} = \delta_{B/A, P} + \delta_{B/A, T} = 0 \quad (\text{constraint})$$

Determine  $\Delta T$  to cause yielding in  $AC$ .

$$-\frac{PL_{AC}}{EA_{AC}} - \frac{PL_{CB}}{EA_{CB}} + L_{AB} \alpha (\Delta T) = 0$$

$$(\Delta T) = \frac{P}{L_{AB} E \alpha} \left( \frac{L_{AC}}{A_{AC}} + \frac{L_{CB}}{A_{CB}} \right)$$

At yielding  $P = A_{AC} \sigma_y$

$$\begin{aligned} (\Delta T)_y &= \frac{A_{AC} \sigma_y}{L_{AB} E \alpha} \left( \frac{L_{AC}}{A_{AC}} + \frac{L_{CB}}{A_{CB}} \right) = \frac{(0.70)(36 \times 10^3)}{(21)(29 \times 10^4)(6.5 \times 10^{-6})} \left( \frac{7}{0.70} + \frac{14}{1.0} \right) \\ &= 152.785^\circ\text{F} \end{aligned}$$

Actual  $\Delta T = 250 - 38 = 212^\circ\text{F} > (\Delta T)_y$ ,  $\therefore$  yielding occurs.

$$\sigma_{AC} = -\sigma_y = -36 \text{ ksi}$$

$$P = \sigma_y A_{AC} = (36 \times 10^3)(0.70) = 25.2 \times 10^3 \text{ lb}$$

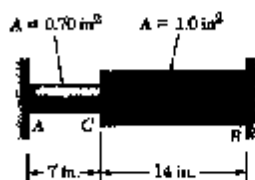
$$\delta_c = -\delta_{C/B} = \frac{PL_{CB}}{EA_{CB}} - L_{CB} \alpha (\Delta T)$$

$$= \frac{(25.2 \times 10^3)(14)}{(29 \times 10^4)(1.0)} - (14)(6.5 \times 10^{-6})(212)$$

$$= 0.012176 - 0.019292 = -0.007116 \text{ in}$$

$$\delta_c = 0.00712 \text{ in}$$

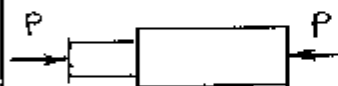
**PROBLEM 2.120**



2.119 The steel rod  $ABC$  is attached to rigid supports and is unstressed at a temperature of  $38^\circ\text{F}$ . The steel is assumed elastoplastic, with  $\sigma_y = 36 \text{ ksi}$  and  $E = 29 \times 10^6 \text{ psi}$ . The temperature of both portions of the rod is then raised to  $250^\circ\text{F}$ . Knowing that  $\alpha = 6.5 \times 10^{-6}/^\circ\text{F}$ , determine (a) the stress in portion  $AC$ , (b) the deflection of point  $C$ .

\*2.120 Solve Prob. 2.119, assuming that the temperature of the rod is raised to  $250^\circ\text{F}$  and then returned to  $38^\circ\text{F}$ .

**SOLUTION**



$$S_{B/A} = S_{B/A,P} + S_{B/A,T} = 0 \quad (\text{constraint})$$

Determine  $\Delta T$  to cause yielding in  $AC$ .

$$-\frac{PL_{AC}}{EA_{AC}} - \frac{PL_{CB}}{EA_{CB}} + L_{AC}\alpha(\Delta T) = 0$$

$$\Delta T = \frac{P}{L_{AC}E\alpha} \left( \frac{L_{AC}}{A_{AC}} + \frac{L_{CB}}{A_{CB}} \right) = \frac{P}{(29 \times 10^6)(6.5 \times 10^{-6})} \left( \frac{7}{0.70} + \frac{14}{1.0} \right)$$

$$= 6.0629 \times 10^{-3} P \quad \text{At yielding } P_y = \sigma_y A_{AC} = (36 \times 10^3)(0.7) = 25.2 \times 10^3 \text{ lb}$$

$$(\Delta T)_y = (6.0629 \times 10^{-3})(25.2 \times 10^3) = 152.785^\circ\text{F}$$

Actual  $\Delta T = 250 - 38 = 212^\circ\text{F} > (\Delta T)_y \therefore$  yielding occurs.

$$\sigma_{AC} = -\sigma_y = -36 \times 10^3 \text{ psi}$$

$$S_c = -S_{B/C} = \frac{PL_{CB}}{EA_{CB}} - L_{CB}\alpha(\Delta T) = \frac{(25.2 \times 10^3)(14)}{(29 \times 10^6)(1.0)} - (14)(6.5 \times 10^{-6})(212)$$

$$= 0.012176 - 0.019292 = -0.007116 \text{ in}$$

Cooling  $\Delta T' = 212^\circ\text{F} \quad P' = \frac{\Delta T}{6.0629 \times 10^{-3}} = \frac{212}{6.0629 \times 10^{-3}}$

$$P' = \frac{\Delta T'}{6.0629 \times 10^{-3}} = \frac{212}{6.0629 \times 10^{-3}} = 34.967 \times 10^3 \text{ lb}$$

(a) Residual stress in  $AC$

$$\sigma_{AC, \text{res}} = -\sigma_y + \frac{P'}{A_{AC}} = -36 \times 10^3 + \frac{34.967 \times 10^3}{0.7} = 13.95 \times 10^3 \text{ psi}$$

$$= 13.95 \text{ ksi}$$

$$S_c' = -S_{B/C}' = -\frac{P'L_{CB}}{EA_{CB}} + L_{CB}\alpha(\Delta T')$$

$$= -\frac{(34.967 \times 10^3)(14)}{(29 \times 10^6)(1.0)} + (14)(6.5 \times 10^{-6})(212)$$

$$= -0.016881 + 0.019292 = 0.002411 \text{ in}$$

$$S_{C,P} = S_c + S_c' = -0.007116 + 0.002411 = -0.00471 \text{ in}$$

$$0.00471 \text{ in} \leftarrow$$